

## **Recent Advances in MRF® Finishing of Large Optics**

*presented to:*

Technology Days in the Government  
Mirror Development  
July 31-August 2 2007

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Acknowledgements:

John West, John Hraba

Dr. Philip Stahl

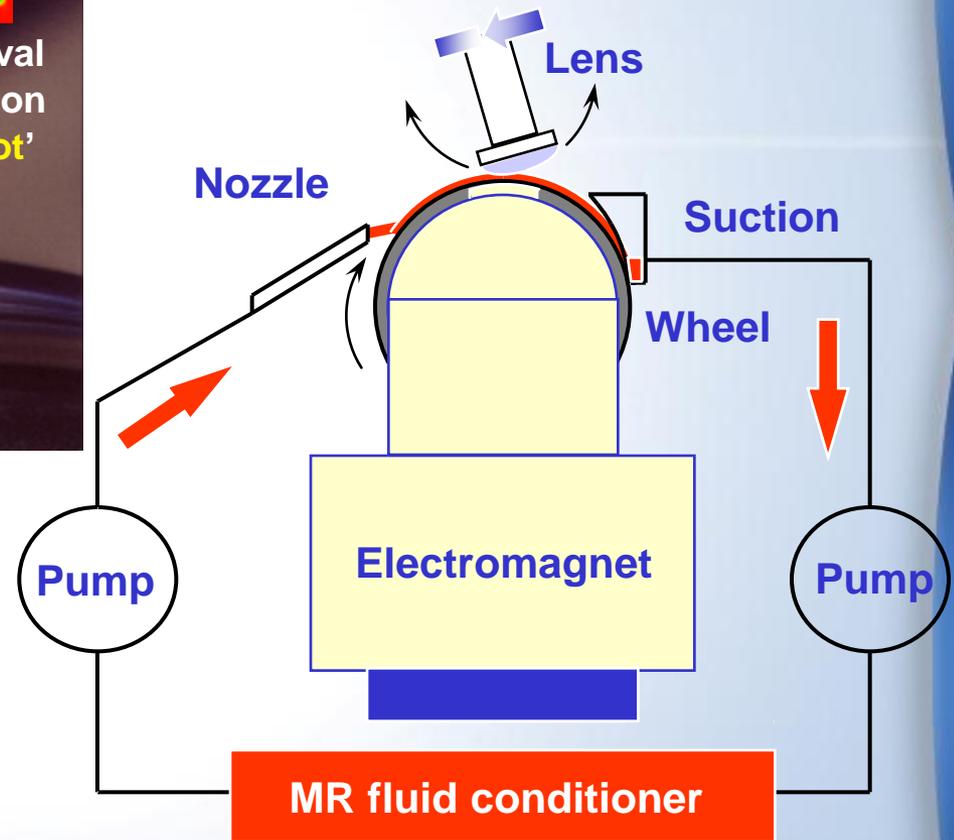
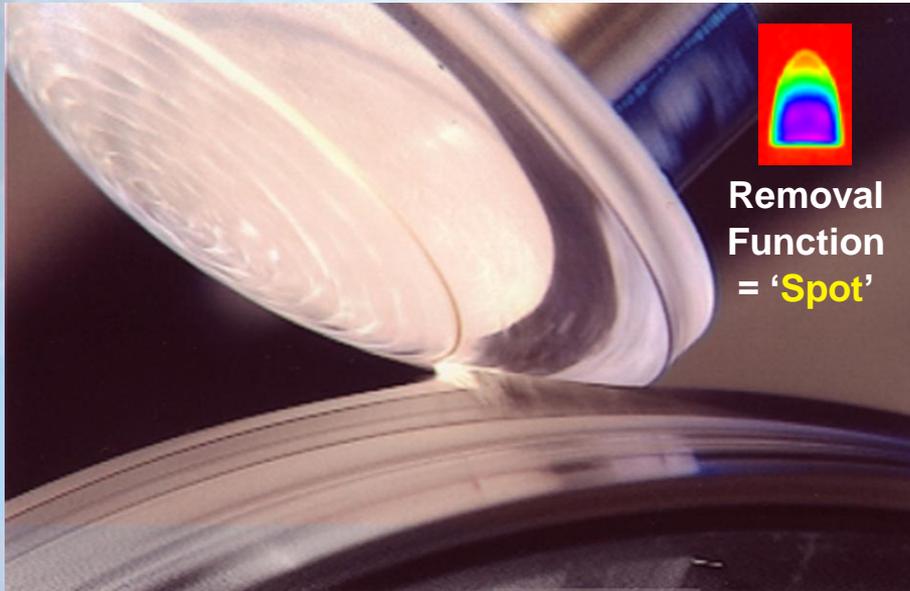
NASA SBIR 03-S2.05-7100

# Outline



- ❖ **Brief MRF<sup>®</sup> technology introduction**
- ❖ **Improved figure correction near edges of large segmented optics using MRF**
- ❖ **Freeform capabilities of large MRF platforms**
- ❖ **Implementation of “pre-polishing” on MRF platforms**

# Magnetorheological Finishing (MRF<sup>®</sup>) – How it works



# MRF – Breakthrough Technology



## The MRF polishing tool:

- never dulls or changes
- is interferometrically characterized
- is easily adjusted
- conforms to part shape - works on complex shapes (flat, sphere, asphere, cylinder, freeform...)
- has high removal rates
- removal based on shear stress so applies very low normal load on abrasive, improving surface integrity
- determinism leads to high convergence rate

These attributes lead to a production-oriented, deterministic, computer-controlled polishing and figuring technique.

Production proven: more than 100 machines worldwide

Polishing optics from 1mm to >1 meter

# Family of QED Machines



- **Q22-XE** – <100 mm in diameter.
- **Q22-X** - Up to 200 mm in diameter.
- **Q22-Y** - Raster tool path, up to 200 mm in size.
- **Q22-400X** - Up to 400 mm in diameter.
- **Q22-750P2** - Plano optics up to 750 mm x 1,000 mm in size.
- **Q22-950F** – Freeform optics up to 950 x 1,250mm
- **Q22-950F-PC**– Freeform optics up to 950 x 1,250mm with pre-polishing capabilities
- **Q22-2000F**– Freeform optics up to 2+ meters
- **SSI<sup>®</sup>** -- Subaperture Stitching Interferometer (SSI) for high precision metrology.
- **SSI-A<sup>®</sup>** -- Subaperture Stitching Interferometer (SSI) for high precision asphere metrology.

# Fabricating Large Segmented Optics using MRF

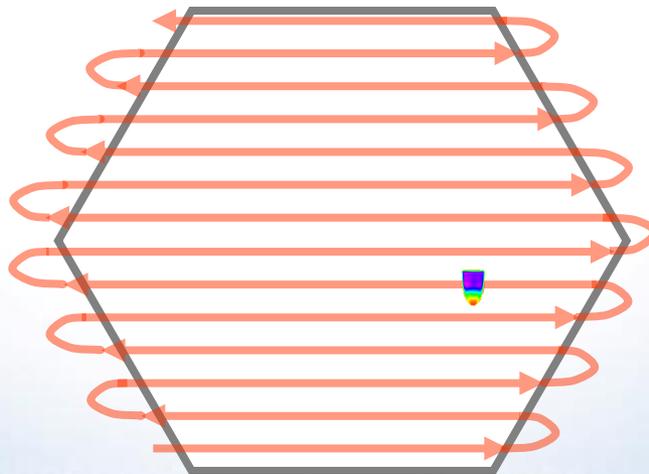


Large segmented mirrors must have little or no edge exclusion

Standard MRF has demonstrated good performance at edges for a variety of aperture sizes and shapes.

Work reported is to improve edges even further.

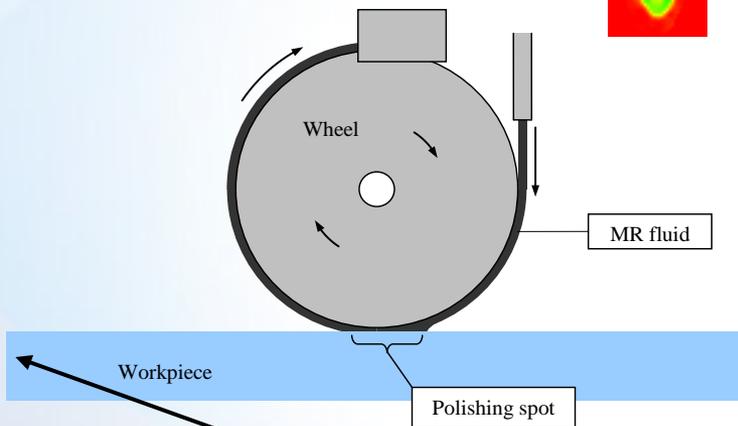
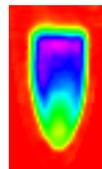
The primary goal of the SBIR is to understand process differences at the edge and to develop an approach to account for them.



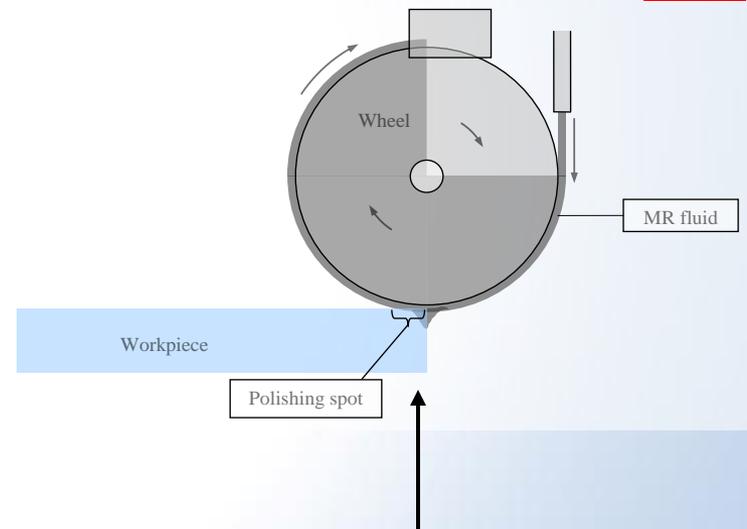
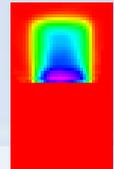
# Causes of Edge Effects

MR fluid flow over edges differs from flow over surface, leading to changes in the tool removal function (“spot”).

Polishing away from edges



Polishing at leading edge



Edge performance at *trailing edge*, superior to *leading edge* due to flow characteristics

# Methods of Eliminating Edge Effects



- ❖ **Removal map biasing: leave edge regions intentionally “high,” and correct with smaller spot**
  - Simplest to implement, but requires additional polishing iterations
- ❖ **Limited tool travel: start or end polishing inside leading or trailing edges, leaving edge regions intentionally “high”**
  - No edge effects at leading or trailing edge
  - Like removal map biasing, requires additional polishing
- ❖ **Variable plunge depth: use a smaller spot near edges**
  - More difficult to implement in software, but should provide best results – potentially in a single polishing iteration
  - Can start or end polishing closer to edges if using limited tool travel

# Removal Map Biasing



Where rolled edges are anticipated, remove less material so that edge regions are intentionally left “high”

- Minimizes amount of material that needs to be removed in subsequent runs

Correct edge regions with a smaller spot with subsequent iteration

Without removal biasing:



Before polishing



Target figure



After polishing

Residual to remove in second run

With removal biasing:



Before polishing



Target figure



After polishing

Residual to remove in second run

# Automatic Edge Bias Map Creation



- ❖ A tool for creating edge bias maps has automatically been added to the MRF Control Software
- ❖ User can also generate customized bias maps

The screenshot displays the MRF Control Software interface. At the top, there is a status bar with fields for Job: S/N: 1, # Runs: 0, 2007-07-18 16:44:23, OK, HOLD, Not Logged On, and Off. The main window shows a color-coded edge bias map of a rectangular wafer with a central purple region and a rainbow-colored border. Below the map, a 'Cross Section' graph plots height in micrometers (µm) against distance from the top in millimeters (mm). The graph shows a flat surface with a slight rise at the edges. The PV is 1.01 and the RMS is 0.223. A dialog box titled 'Create Edge Bias Map' is open, allowing for customization of bias and extent for the Top, Bottom, Left, and Right edges. The dialog box has a close button (X) in the top right corner. The 'Top Edge' settings are Bias (µm): 0.5 and Extent (mm): 20. The 'Bottom Edge' settings are Bias (µm): 1 and Extent (mm): 25. The 'Left Edge' settings are Bias (µm): -0.1 and Extent (mm): 10. The 'Right Edge' settings are Bias (µm): -0.1 and Extent (mm): 10. At the bottom of the dialog box are 'OK' and 'Cancel' buttons. The main software interface also has 'Main Menu', 'Run Job', and 'Define Job' buttons at the bottom, and a 'QED' logo in the bottom right corner.

Job: S/N: 1 # Runs: 0 2007-07-18 16:44:23 OK HOLD  
Not Logged On Off

1) Is the DESIRED FINAL FIGURE something other than perfect?  
No

2) Load Desired Final Figure  
Load Metrology File name

Visible Width Visible Height Pixel Scale

PV: 1.1 RMS: 0.238  
-0.1 µm 1

Cross Section  
µm  
-0.1 1  
0 distance from top (mm) 200  
PV: 1.01 RMS: 0.223

Define Job ( 5 / 8 ) |<<

Main Menu Run Job Define Job

QED

**Create Edge Bias Map**

Top Edge  
Bias (µm): 0.5  
Extent (mm): 20

Bottom Edge  
Bias (µm): 1  
Extent (mm): 25

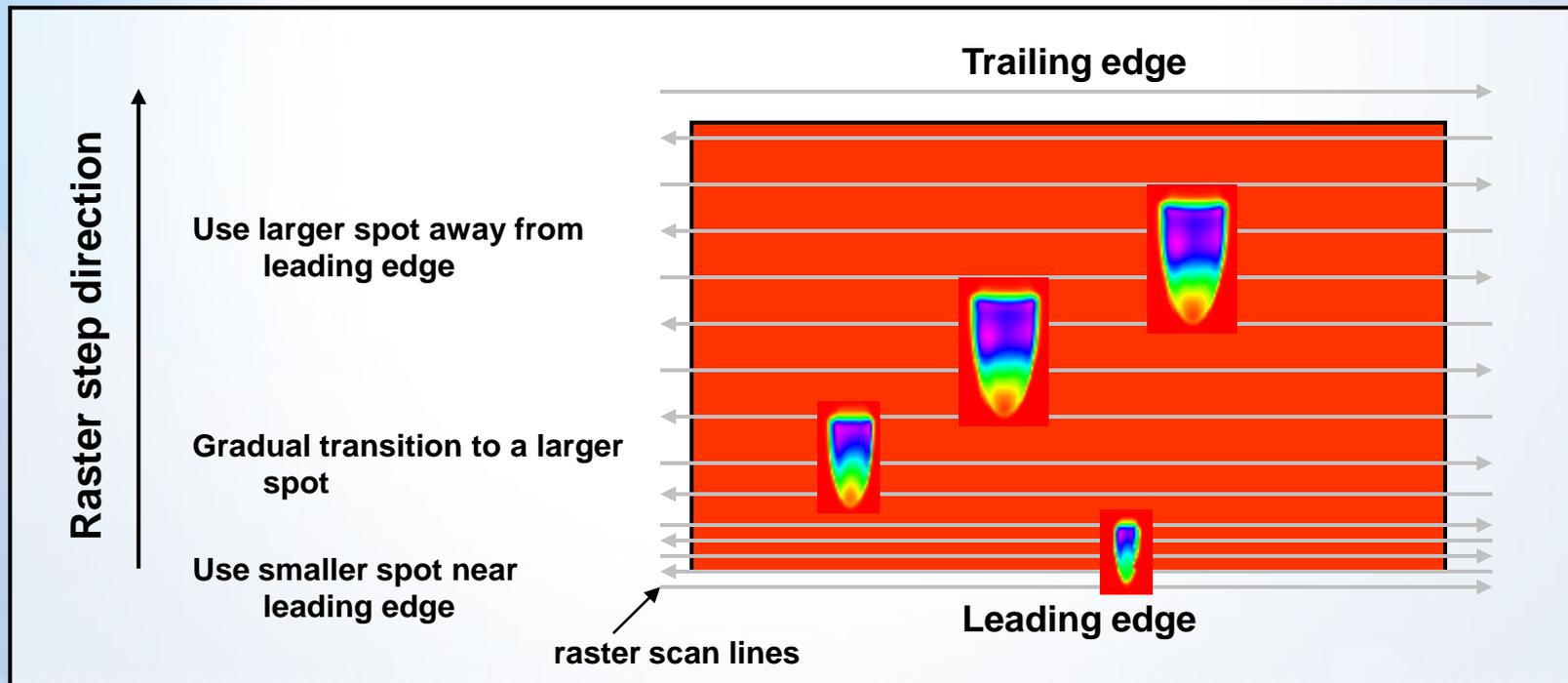
Left Edge  
Bias (µm): -0.1  
Extent (mm): 10

Right Edge  
Bias (µm): -0.1  
Extent (mm): 10

OK Cancel

# Variable Plunge Depth

- ❖ Extent of edge effect is proportional to spot size, but polishing time is (roughly) inversely proportional to spot size
- ❖ Use smaller spot (lower plunge depth) near edges where edge effects are anticipated; use larger spot (higher plunge depth) away from edges to remove material quickly

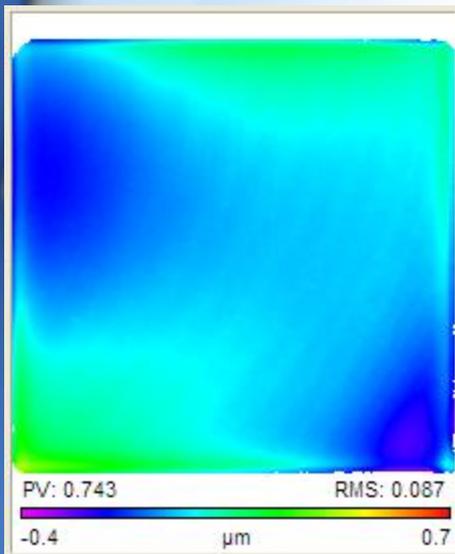


# Process Example

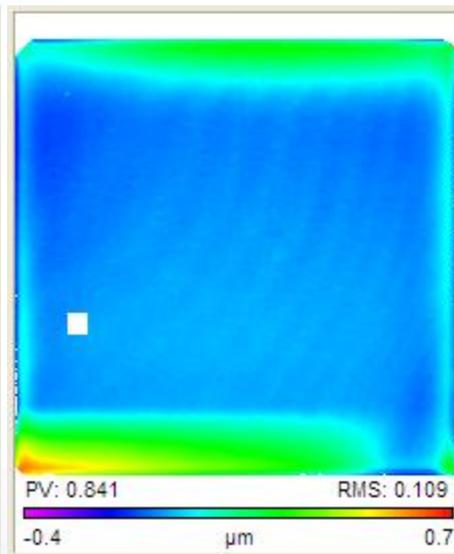


## Two polishing runs on 74 x 74 mm CA part:

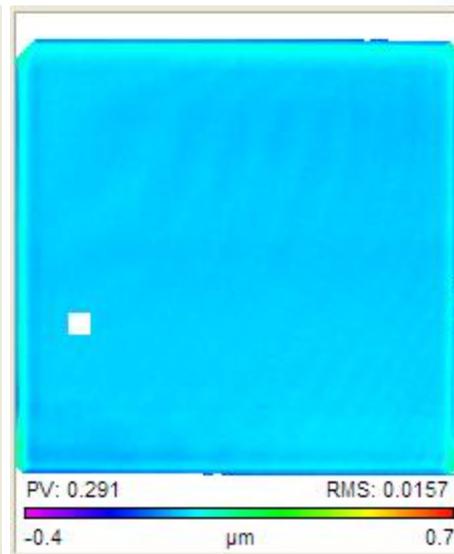
- Polishing using large MRF wheel (370 mm diameter used on meter-class platforms) to perform low-order correction
- Standard polishing run using small wheel (50 mm) to correct higher spatial frequency features



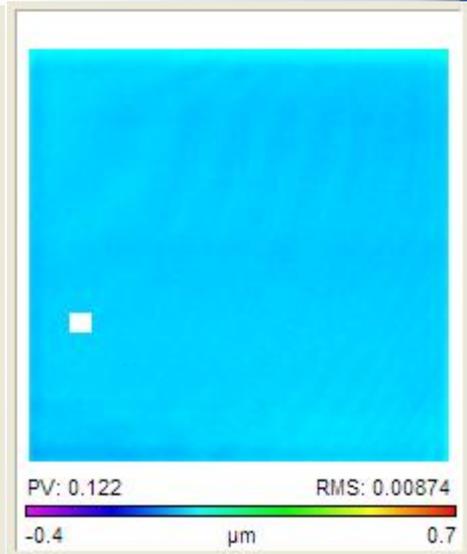
Initial surface  
0.74 µm PV  
0.087 µm RMS



After 370 mm wheel run  
Corrected low-order figure  
away from edges



After 50 mm wheel run  
(full clear aperture)  
0.29 µm PV  
0.016 µm RMS



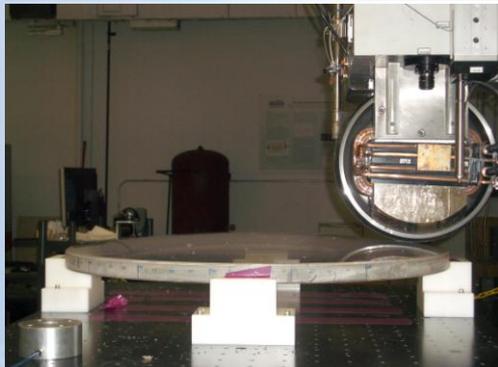
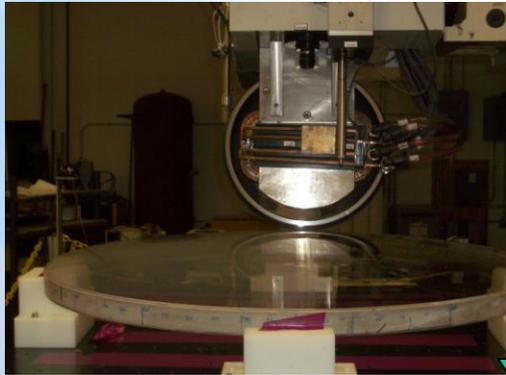
After 50 mm wheel run (2  
mm edge exclusion)  
0.13 µm PV  
0.0087 µm RMS

# Polishing Cycle Time

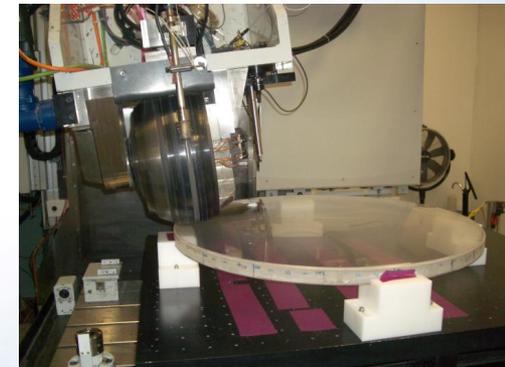
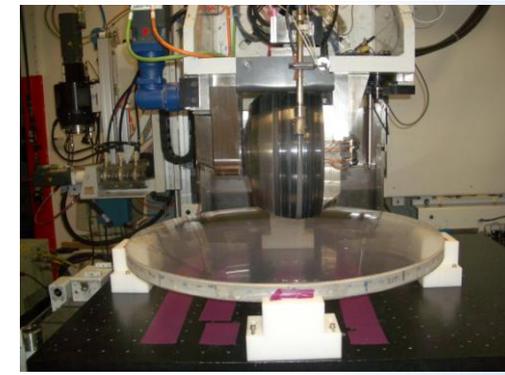
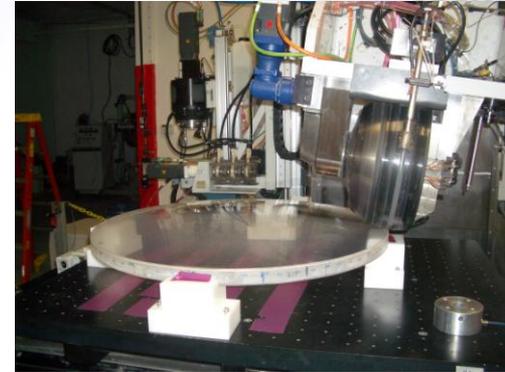


- ❖ For the multi-run polishing approach to be advantageous, the polishing cycle time must be significantly less than those of using a single small spot
- ❖ Estimated cycle time for polishing using 50 mm wheel only was 35% longer than using a multi-run approach.
- ❖ *Time savings are much greater for larger parts since a smaller fraction of the surface area is within one spot length or width of the edges*

# Q22-950F Freeform Machine

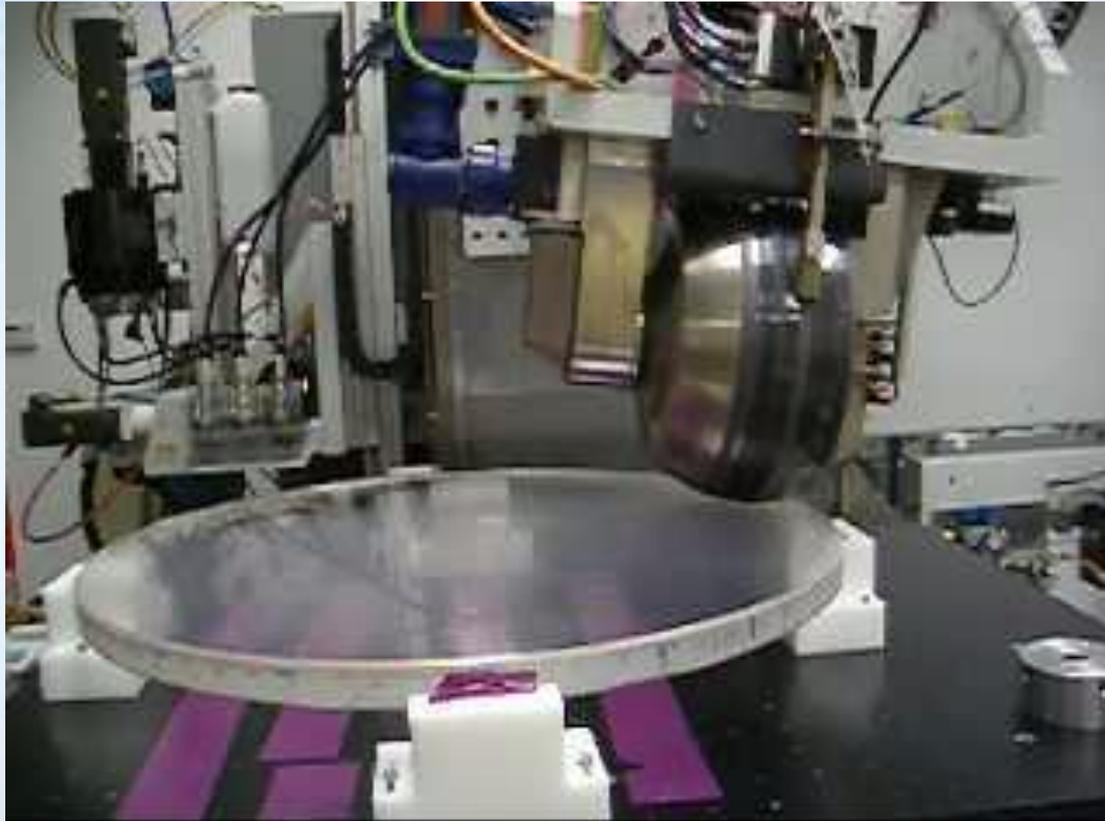


Polishing around the wheel



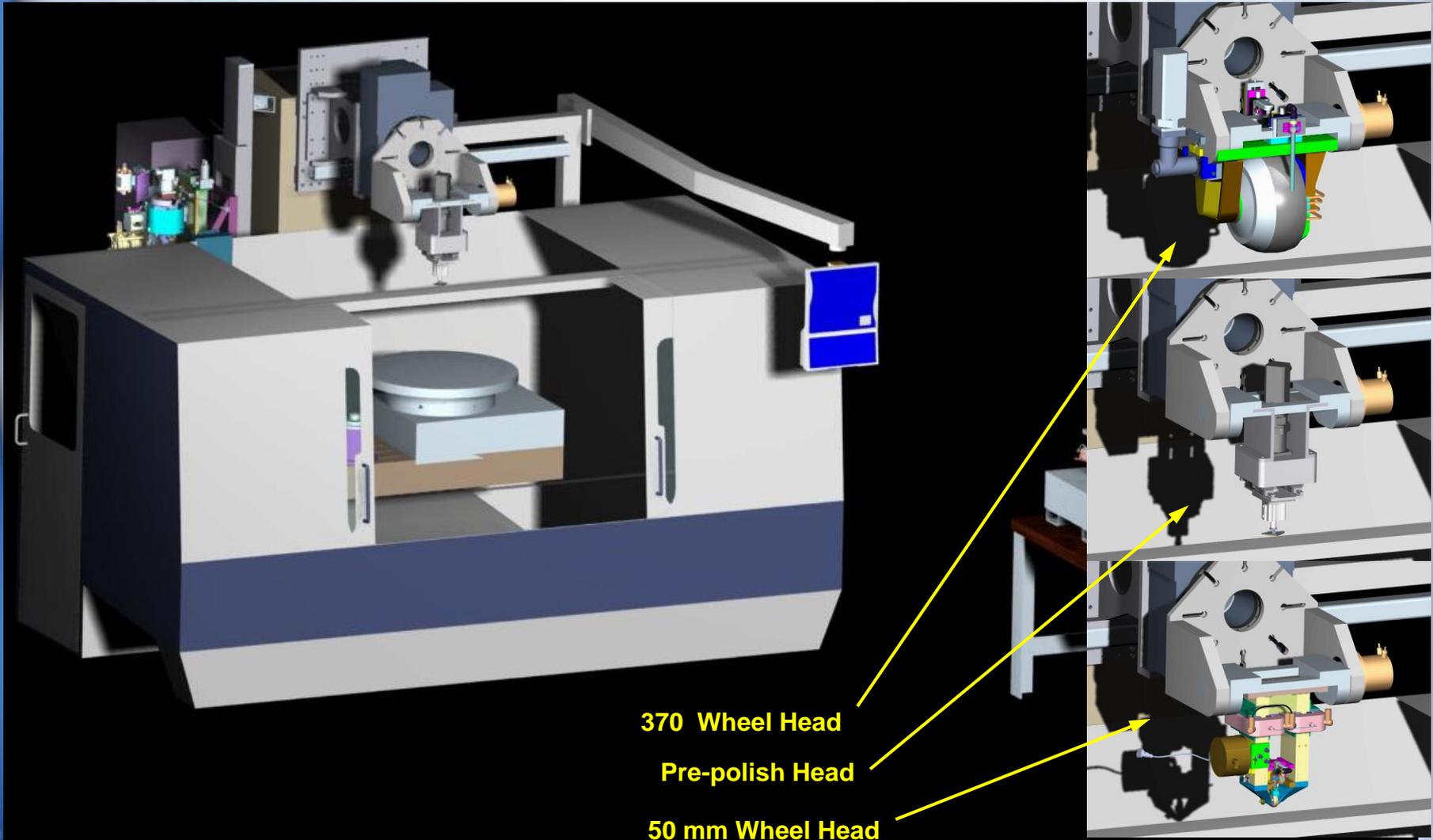
C-axis pivot

# Raster Polishing Large Aperture Aspheres



- ❖ 840 mm diameter
- ❖ Fused silica
- ❖ 1.3 mm departure from best fit sphere

# Q22-950F Polishing Center

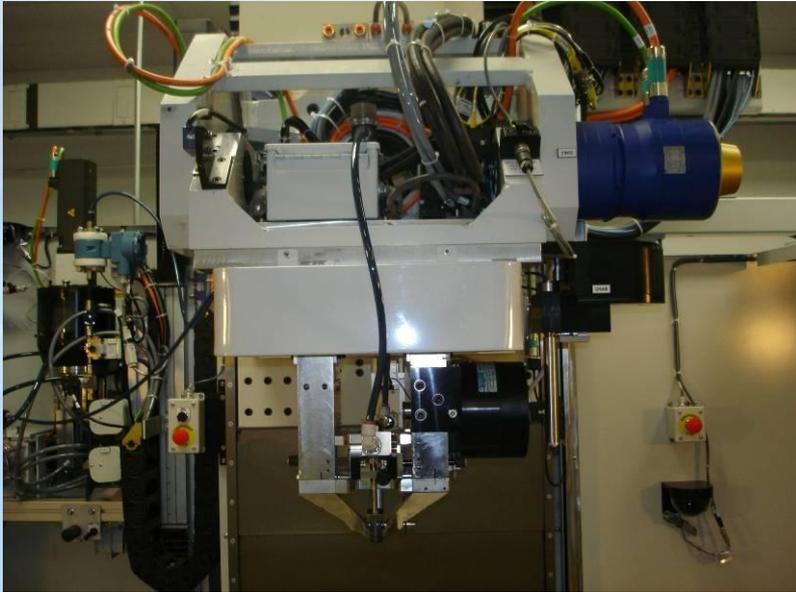


370 Wheel Head

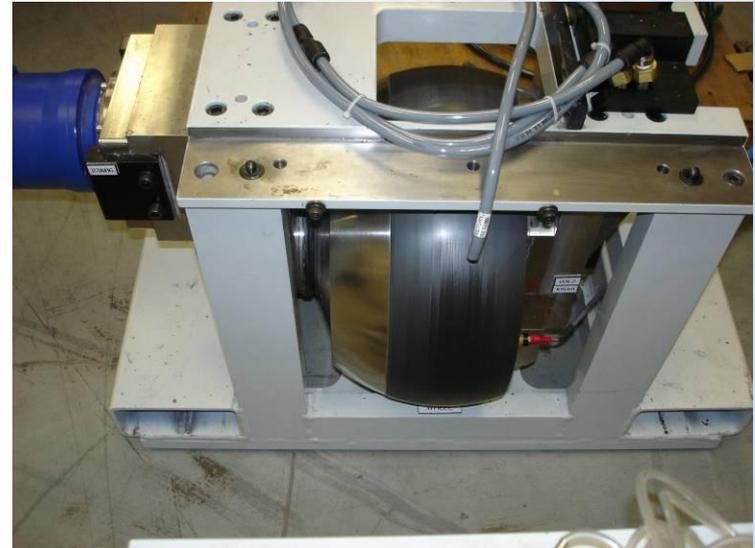
Pre-polish Head

50 mm Wheel Head

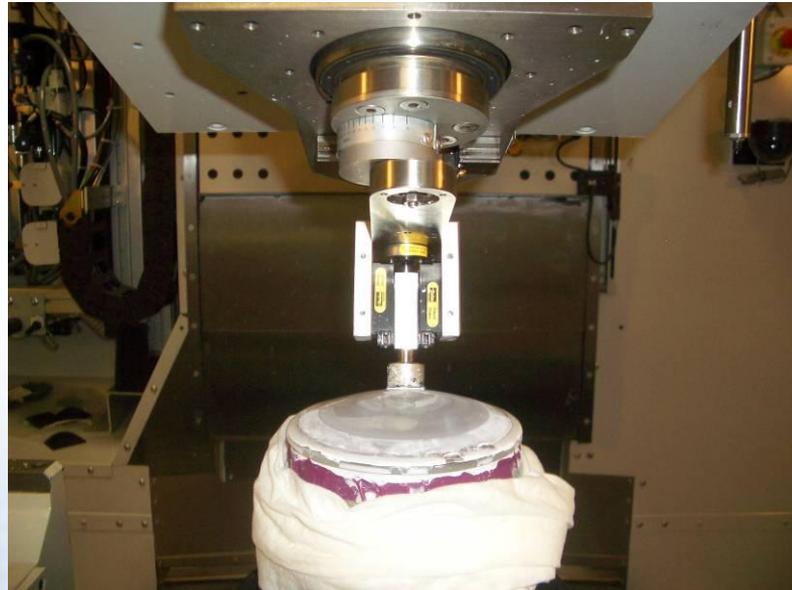
# Three Heads



**Ø50mm MRF**

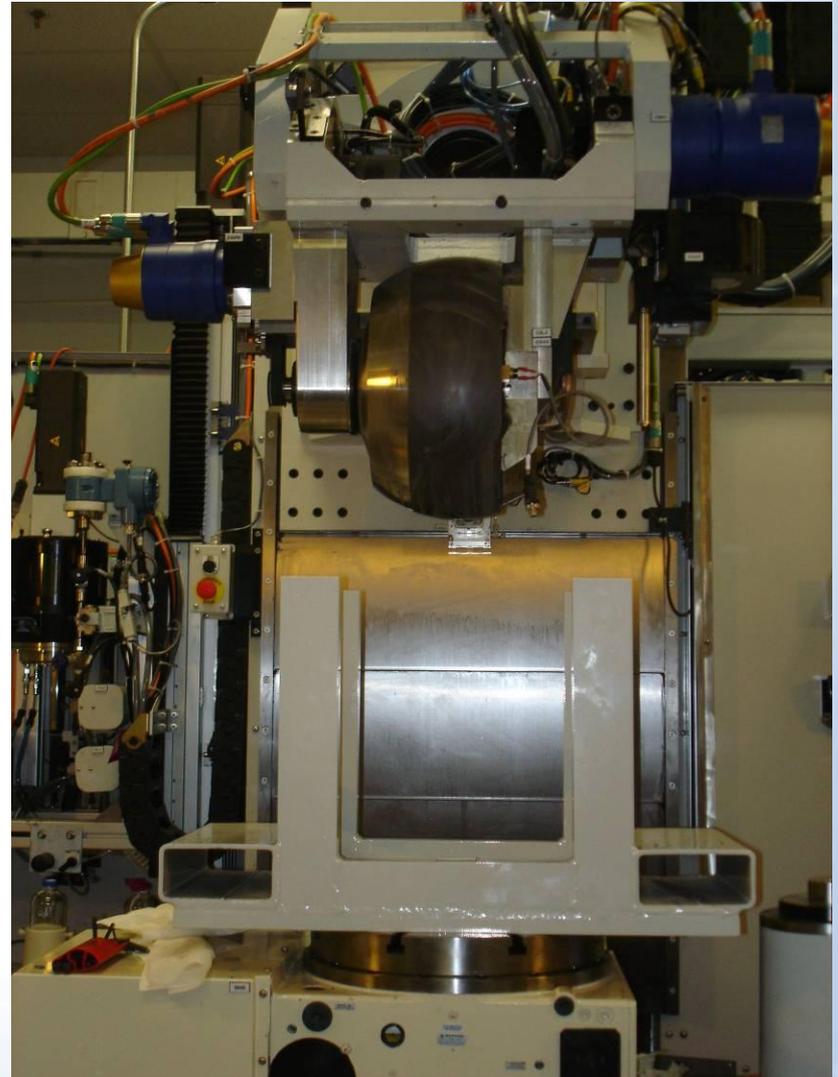
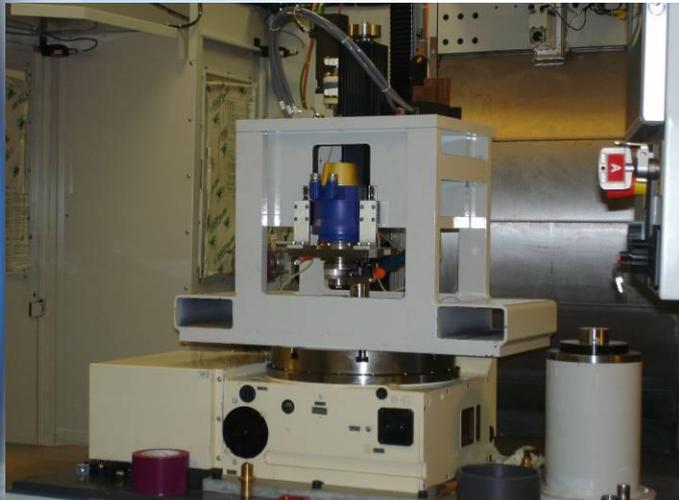
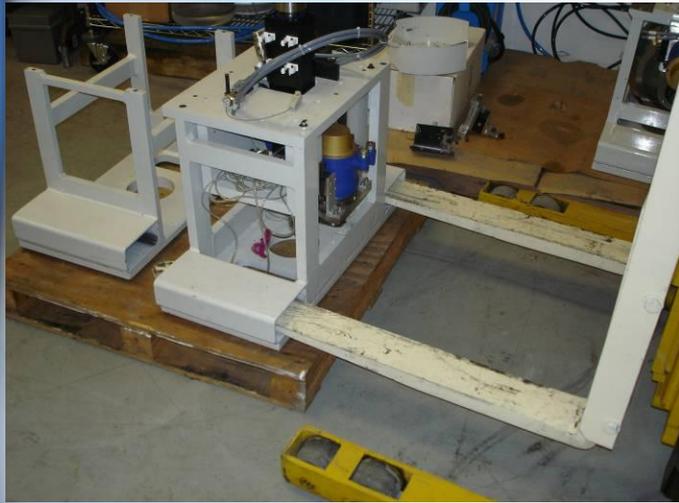


**Ø370mm MRF**

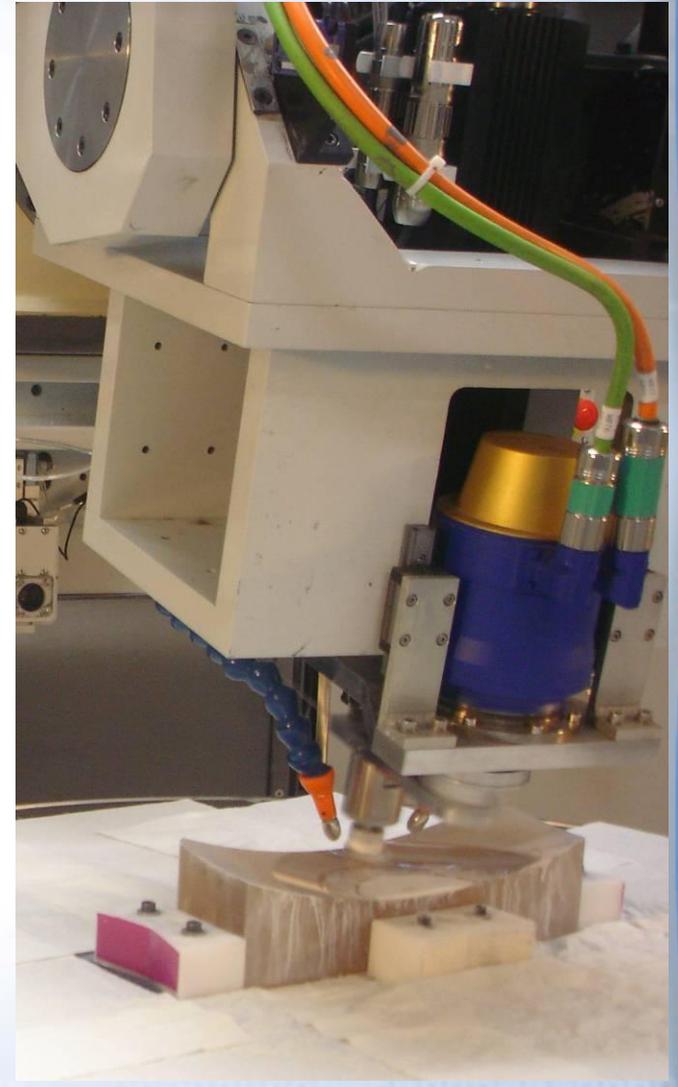
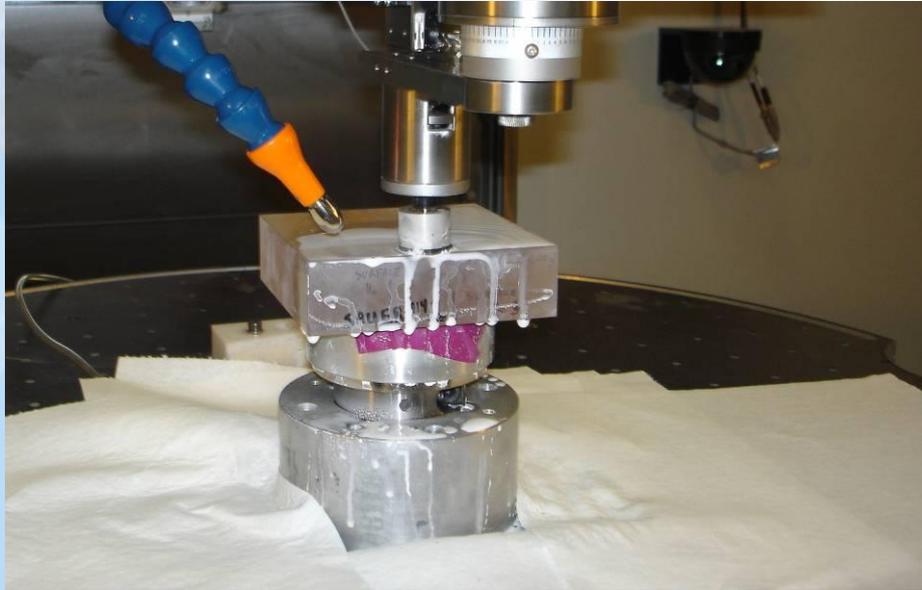


**Pre-Polishing Head**

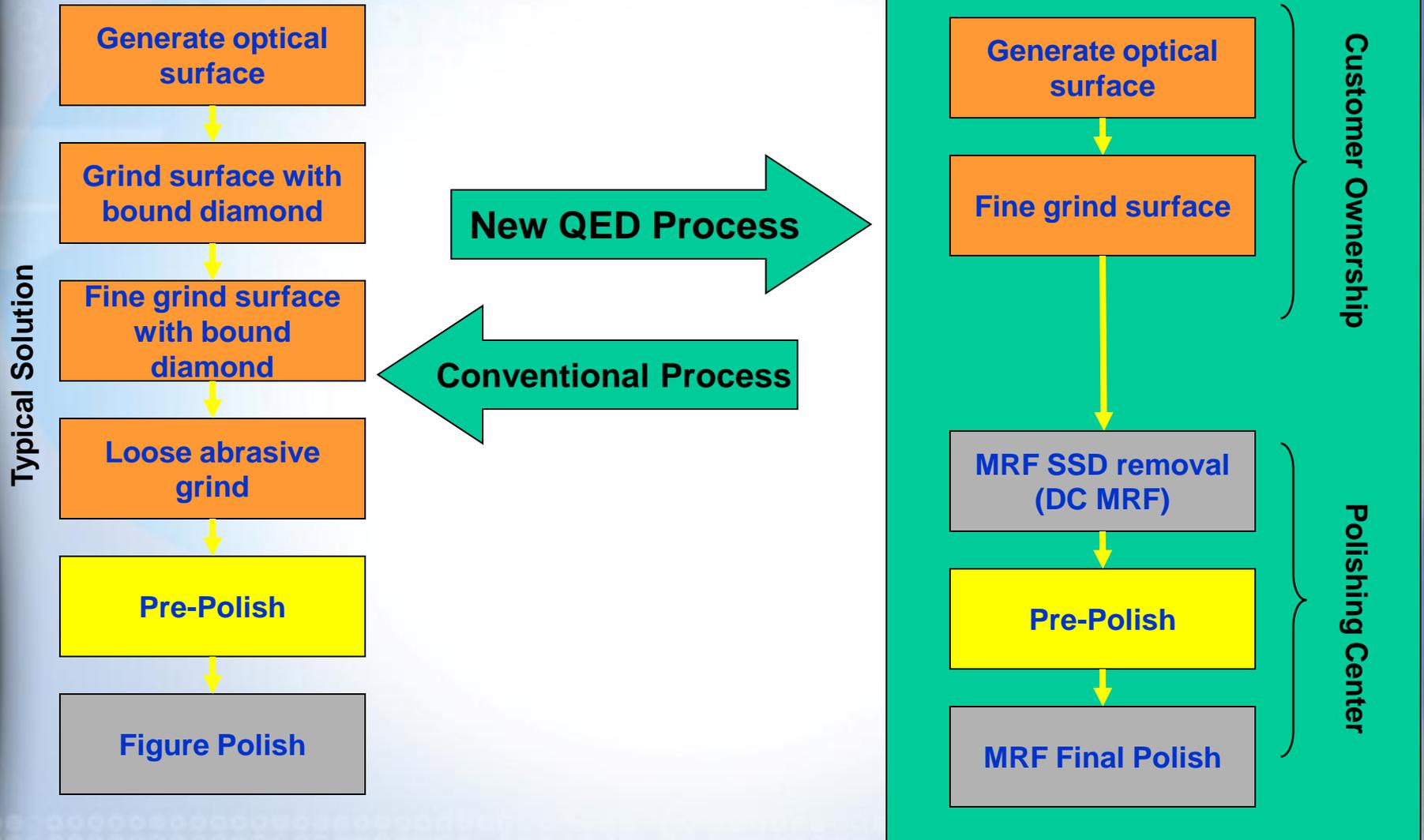
# Changing Heads



# Pre-Polishing Head



# Novel Process Flow



# Example: Off-axis Component



~300 x 90 mm off-axis spherical section

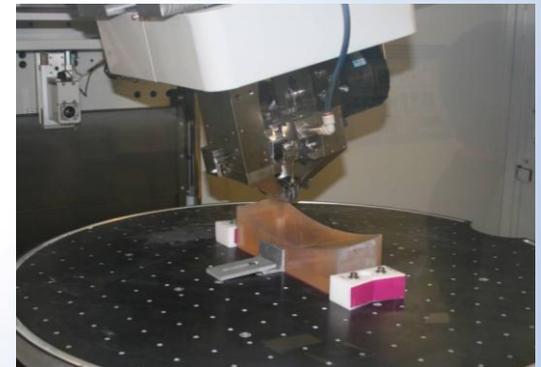
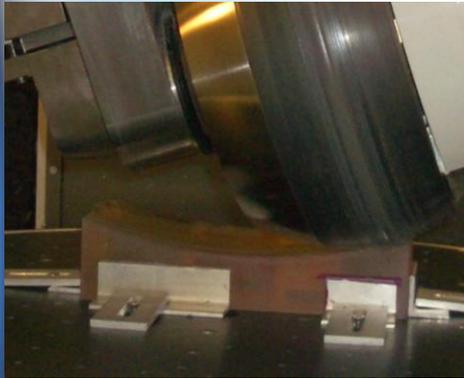
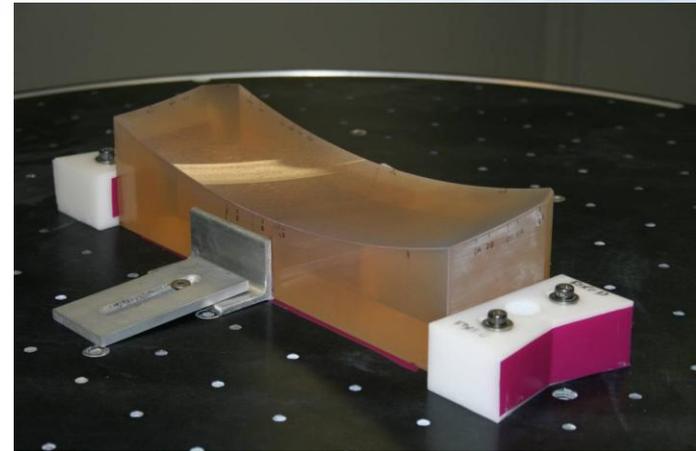
~286 x 72 mm Clear Aperture

$R = -450$  mm (cc)

Zerodur

Process on Q22-950 PC

- MRF Damage Removal
- Smoothing (sub-ap pitch tool)
- MRF Figure Correction



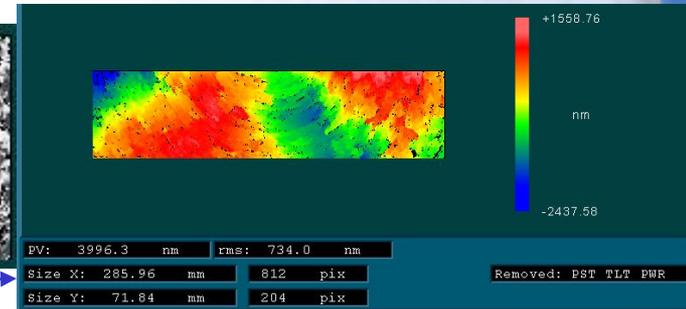
# Off-axis process development Component



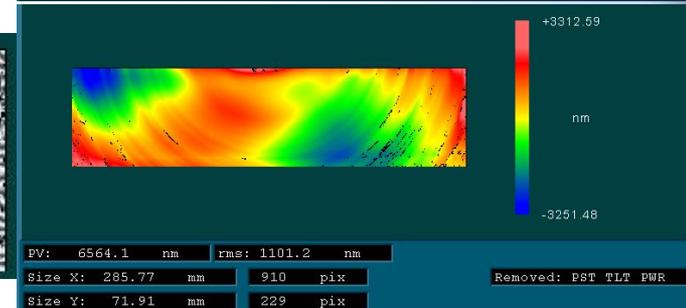
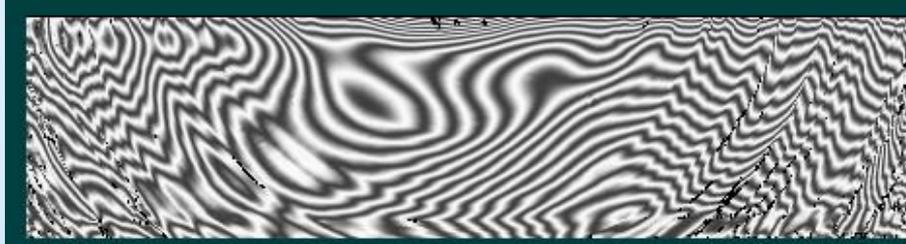
Initial Condition – Figure could not be measured at all until after MRF damage removal

After MRF  
Damage  
Removal

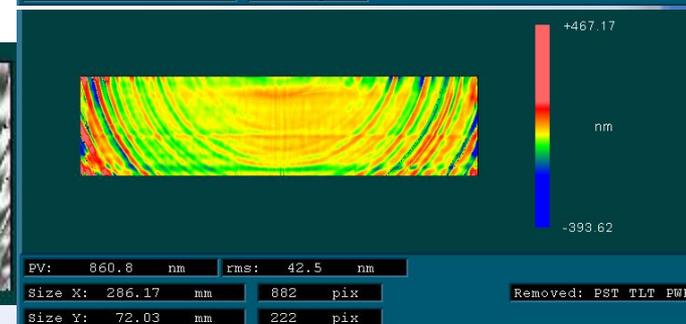
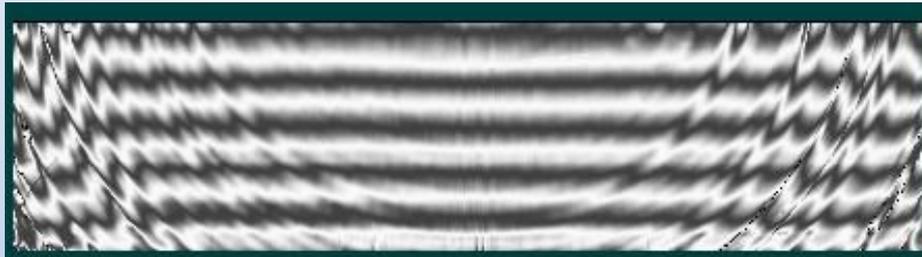
Uncertainty in PV & RMS is high because high slopes from grinding marks cause high fringe density



After Pad  
Polish



After MRF  
figure  
correction



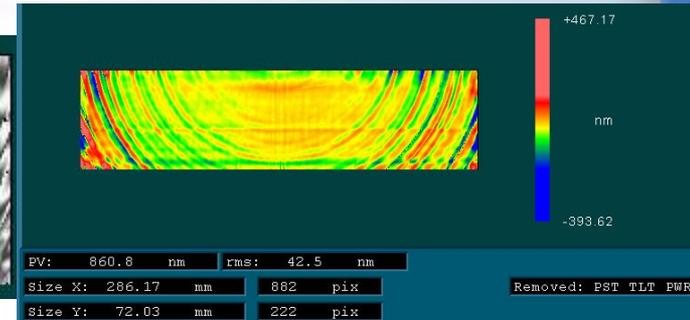
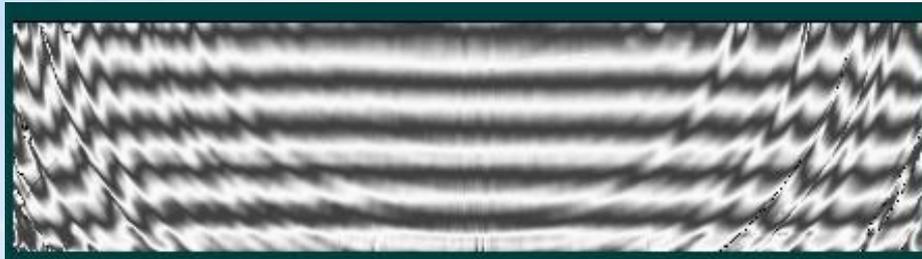
All Data shown over 286 x 72 mm CA

# Off-axis process development Component

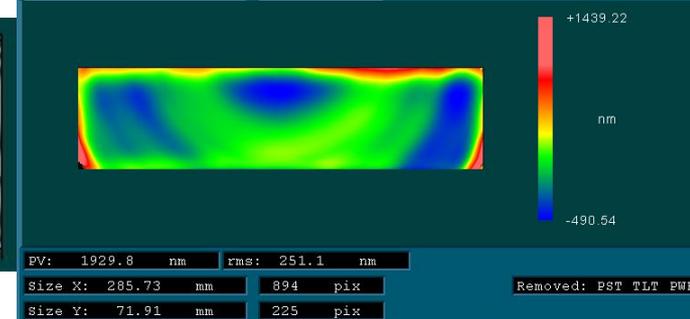
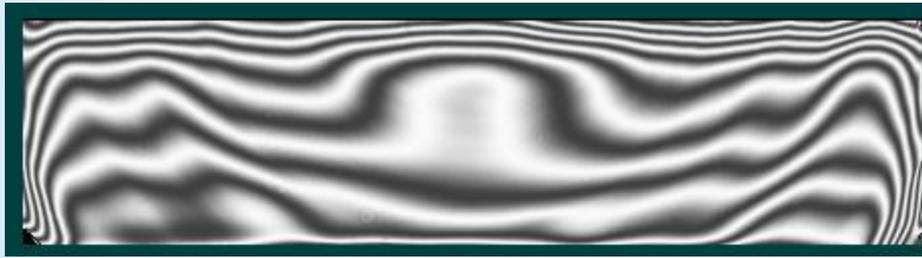


After 2nd Round of Pad/MRF

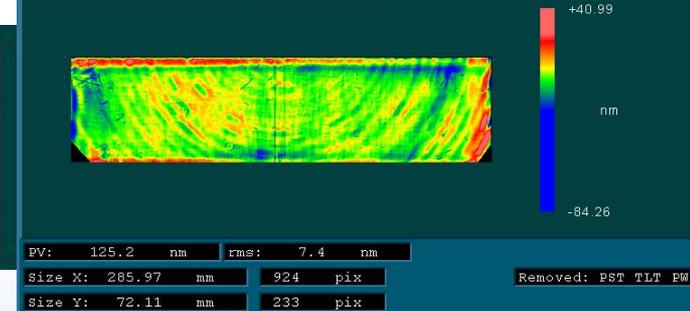
After 1st  
MRF FC



After  
Additional  
Pad  
Polish



After 2nd  
MRF FC

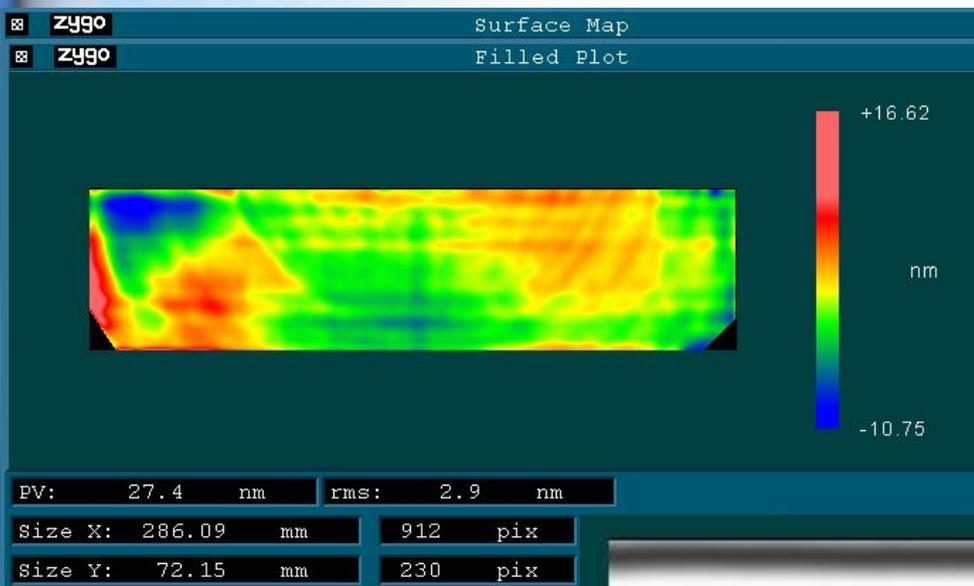


# Off-axis Component - Final Figure



## Final Measurement

(Only Piston, Tilt & Power Removed)



**PV = 27.4 nm**

**( $\lambda/23$ )**

**RMS = 2.9 nm**

**( $\lambda/218$ )**

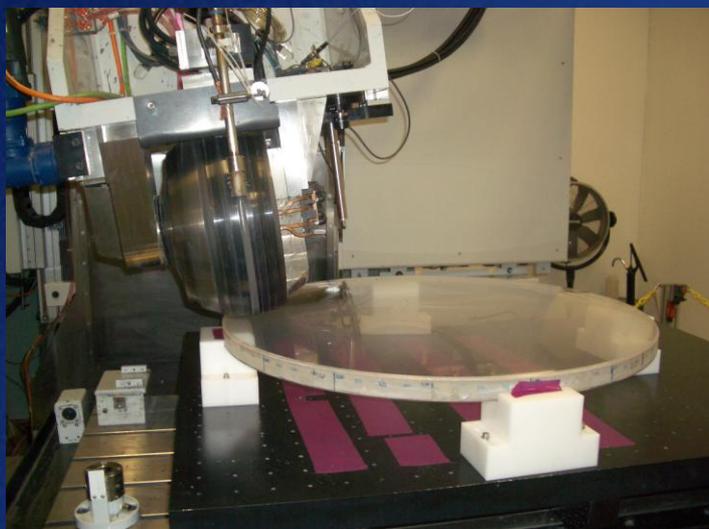
**Synthetic Fringes**



# Summary



- ❖ **Methods have been demonstrated to improve the surface figure near edges of large segmented optics using MRF.**
- ❖ **MRF platforms have been developed that are capable of polishing 1 meter and larger apertures with freeform geometries.**
- ❖ **A pre-polishing process has been implemented on QED platforms to work in accord with the MRF process.**



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